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METHOD AND APPARATUS FOR BALANCING RESISTANCE

Field of the Invention

The present invention is directed to resistance balancing, and more particularly to a
5 mass flow sensor that is capable of detecting the mass flow rate of a fluid by balancing the
resistance of upstream and downstream temperature sensors.

Description of Related Art

Mass flow sensors are used in a wide variety of applications to measure the mass flow
10 rate of a gas or other fluid. One application in which a mass flow sensor may be used is a
mass flow controller. In a conventional mass flow controller, the mass flow rate of a fluid
flowing in a main fluid flow path is regulated or controlled based upon a mass flow rate of a
portion of the fluid that is diverted into a typically smaller conduit forming a part of the mass
flow sensor. Assuming laminar flow in both the main flow path and the conduit of the
15 sensor, the mass flow rate of the fluid flowing in the main flow path can be determined (and
regulated or controlled) based upon the mass flow rate of the fluid flowing through the
conduit of the sensor.

Two different types of mass flow sensors have traditionally been used, constant
current mass flow sensors, and constant temperature mass flow sensors. An example of a
20 constant current mass flow sensor is illustrated in Fig. 1. In Fig. 1, a fluid flows in a sensor
pipe or conduit in the direction of the arrow X. Heating resistors or "coils" R_1 and R_2 having
a large thermal coefficient of resistance are disposed about the sensor conduit on downstream
and upstream portions of the sensor conduit, respectively, and are provided with a constant
current I from a constant current source 901. As a result of the constant current I flowing
25 through the coils R_1 and R_2 , voltages V_1 and V_2 are developed across the coils. The
difference between voltages V_1 and V_2 ($V_1 - V_2$) is taken out of a differential amplifier 902,
with the output of the amplifier 902 being proportional to the flow rate of the fluid through
the sensor conduit.

At a zero flow rate, the circuit of Fig. 1 is configured so that the resistance value (and
30 thus, the temperature) of coil R_1 is equal to the resistance value (and temperature) of coil R_2 ,
and the output of the amplifier 902 is zero. As fluid flows in the sensor conduit, heat that is
generated by coil R_2 and imparted to the fluid is carried towards R_1 . As a result of this fluid
flow, the temperature of coil R_2 decreases and that of coil R_1 increases. As the voltage
dropped across each of these resistors is proportional to their temperature, voltage V_1

increases with an increased rate of fluid flow and voltage V_2 decreases, with the difference in voltage being proportional to the mass rate of flow of the fluid through the sensor conduit.

An advantage of a constant current mass flow sensor is that it can operate over a wide range of temperatures, is relatively simple in construction, and is responsive to changes in the ambient temperature of the fluid entering the sensor conduit. In this regard, as the ambient temperature of the fluid entering the sensor conduit changes, so does the resistance of each of the coils R_1 and R_2 . However, it takes a relatively long time for the temperature (and thus, the resistance) of the coils R_1 and R_2 to stabilize in response to a change in the rate of flow of the fluid.

The other type of mass flow sensor that is frequently used is a constant temperature mass flow sensor, examples of which are illustrated in Figs. 2-4. As shown in the constant temperature mass flow sensor of Fig. 2, heating resistors or "coils" R_{1a} and R_{1b} are respectively disposed about the downstream and upstream portions of a sensor conduit through which a fluid flows in the direction of the arrow X. As in the constant current mass flow sensor of Fig. 1, each of the downstream and upstream coils R_{1a} and R_{1b} has a large thermal coefficient of resistance. The resistance (and thus the temperature) of each of the coils R_{1a} , R_{1b} is fixed by separate and independent circuits to the same predetermined value that is governed by the value of resistors R_{2a} , R_{3a} , R_{4a} , and R_{2b} , R_{3b} , R_{4b} , respectively. Control circuitry is provided to maintain each of the coils R_{1a} , R_{1b} at the same predetermined value of resistance (and thus, temperature) independently of the rate of fluid flow through the sensor conduit.

In the absence of fluid flow, the circuit of Fig. 2 is configured so that the resistance (and temperature) of each of the downstream and upstream coils R_{1a} and R_{1b} is set to the same predetermined value and the output of the circuit is zero. As fluid flows in the sensor conduit, heat from the upstream coil R_{1b} is carried towards R_{1a} . As a result, less energy is required to maintain the downstream coil R_{1a} at the fixed temperature than is required to maintain the upstream coil R_{1b} at that same fixed temperature. The difference in energy required to maintain each of the coils R_{1a} , R_{1b} at the predetermined temperature is measured and is proportional to the mass flow rate of fluid flowing through the sensor conduit.

The constant temperature mass flow sensor described with respect Fig. 2 is also relatively easy to construct. In addition, the circuit of Fig. 2 stabilizes more quickly in response to changes in the mass flow rate of the fluid entering the sensor conduit than the constant current mass flow sensor described with respect to Fig. 1. However, because each of

the coils R_{1a} and R_{1b} is set and maintained at a predetermined temperature independently of the ambient temperature of the fluid flowing into the sensor conduit, a problem arises when the ambient temperature of the fluid flowing into the sensor conduit increases. In particular, when the ambient temperature of the fluid flowing in the sensor conduit approaches the predetermined temperature that is maintained by the upstream and downstream coils, the circuit loses its ability to discern differences in the flow rate of the fluid, and when the ambient temperature of the fluid increases beyond this predetermined temperature, the sensor is rendered inoperable.

To overcome these disadvantages, a number of alternative constant temperature mass flow sensors have been provided. For example, the circuit of Fig. 3 provides a constant temperature mass flow sensor that is capable of responding to changes in the ambient temperature of a gas or fluid, at least to a certain degree. Once again, R_{1b} and R_{2b} are downstream and upstream temperature sensing coils with a large temperature coefficient of resistance. However, rather than maintaining the temperature of the coils at a predetermined constant value as in the circuit of Fig. 2, the circuit of Figure 3 maintains the temperature of the sensor coils R_{1b} , R_{2b} at a temperature that is above the ambient temperature of the fluid flowing into the sensor conduit. This is achieved by the insertion of an additional coil R_{3b} , R_{4b} having a coefficient of resistance similar to that of the sensor coils R_{1b} , R_{2b} in each of the downstream and upstream circuits. As the ambient temperature of the fluid changes, the series addition of coil resistance R_{3b} , R_{4b} to the temperature setting resistors R_{5b} , R_{6b} results in raising the temperature to which the upstream and downstream resistance coils are maintained above the ambient temperature of the fluid flowing into the sensor conduit. As in the circuit of Fig. 2, the difference in energy supplied by each of the downstream and upstream circuits to maintain the temperature of the coils R_{1b} , R_{2b} at the same temperature is proportional to the mass flow rate of the fluid through the sensor conduit.

As should be appreciated by those skilled in the art, for the circuit of Fig. 3 to operate properly, it is critical that the values and thermal characteristics of each element in the downstream circuit match that of the corresponding element in the upstream circuit. Thus, the resistance of the downstream and upstream coils R_{1b} , R_{2b} must have the same value, and the same thermal coefficient of resistance. In addition, resistor R_{3b} must have the same value and the same (ideally large) thermal coefficient of resistance as resistor R_{4b} , resistor R_{5b} must have the same value and same (ideally zero) thermal coefficient of resistance as resistor R_{6b} , resistor R_{7b} must have the same value and same (ideally zero) thermal coefficient of

resistance as resistor R_{10b} , resistor R_{9b} must have the same value and same (ideally zero) thermal coefficient of resistance as resistor R_{8b} , and amplifiers 911 and 912 must have the same operating and temperature characteristics.

Despite the addition of resistors R_{3b} and R_{4b} , a problem with the circuit of Fig. 3 is that as the ambient temperature of the fluid flowing into the sensor conduit rises, the sensor becomes less accurate because the proportional difference between the temperature of the upstream and downstream coils relative to the temperature of the ambient fluid becomes smaller. Further, there is a problem due to drift in that the calibration of the sensor at one temperature does not necessarily allow its use at other ambient temperatures without some sort of compensation circuit.

To solve some of the aforementioned problems, U.S. Patent No. 5,401,912 proposes a constant temperature rise (above ambient) mass flow sensor, an example of which is shown in Fig. 4. The circuit of Fig. 4 acts to maintain upstream and downstream sensor coils R_2 , R_1 at a predetermined value above the ambient temperature of the fluid flowing into the sensor conduit. The circuit of Fig. 4 is identical to the circuit of Fig. 2, except that the fixed value resistors R_{3a} and R_{3b} of Fig. 2, which have an essentially zero thermal coefficient of resistance, are replaced with resistors R_5 and R_6 , respectively, having a large and specific valued thermal coefficient of resistance. As a result of these changes, the circuit of Fig. 4 purportedly maintains a constant temperature rise over the ambient temperature of the fluid flowing into the sensor conduit. Such a mass flow sensor as is shown in Fig. 4 is therefore termed a constant temperature difference (over ambient) or a constant temperature rise (over ambient) mass flow sensor.

Each of the aforementioned constant temperature mass flow rate sensors utilizes separate and independent upstream and downstream circuits to set the temperature of the upstream and downstream coils to a particular value, or to a particular value over the ambient temperature of the fluid flowing into the sensor conduit. A disadvantage of each of these circuits is that they require a close matching of corresponding circuit elements (i.e., resistors, coils, and amplifiers) in the upstream and downstream circuits.

Summary of the Invention

According to one embodiment of the present invention, a sensor is provided that includes a first resistor, a second resistor, a first circuit, and a second circuit. The first and second resistors each has a resistance that varies in response to a change in a physical

property. The first circuit is electrically coupled to the first resistor and sets the resistance of the first resistor. The second circuit is electrically coupled to the second resistor and adjusts the resistance of the second resistor to equal the resistance of the first resistor. A processing circuit may be coupled to the first and second circuits to measure a difference in an amount of energy provided by the first and second circuits to the first and second resistors, respectively. Where the resistance of the first and second resistors varies in response to a change in temperature, and the first and second resistors are disposed about a conduit in which fluid flows, the sensor is capable of measuring a mass flow rate of the fluid flowing in the conduit.

According to another embodiment of the present invention, a mass flow sensor is provided. The sensor includes a first heat sensitive coil, a second heat sensitive coil, a first circuit, a second circuit, and a processing circuit. The first and second heat sensitive coils are disposed at spaced apart positions about a conduit through which a fluid flows, and each has a resistance that varies with temperature. The first circuit is electrically coupled to the first heat sensitive coil and sets the resistance of the first heat sensitive coil to a value that corresponds to a predetermined temperature. The second circuit is electrically coupled to the second heat sensitive coil and adjusts an amount of current provided to the second heat sensitive coil so that the resistance of the second heat sensitive coil equals the resistance of the first heat sensitive coil. The processing circuit is coupled to the first and second circuits and measures a difference in an amount of energy provided by the first and second circuits to the first and second heat sensitive coils, respectively.

According to a further embodiment of the present invention, a method of balancing a resistance of a first resistor and a resistance of a second resistor is provided. The resistance of the first and second resistors vary with temperature, and the method includes acts of setting the resistance of the first resistor to a first value and providing an amount of current to the second resistor so that the resistance of the second resistor matches the first value of the first resistor.

According to another embodiment of the present invention, a method of setting the resistance of a resistor is provided. The method includes acts of: (a) measuring an ambient temperature of a fluid flowing into a conduit about which the resistor is disposed, (b) incrementing the ambient temperature measured in act (a) by a predetermined amount to identify a temperature to which the resistor is to be set, (c) calculating a value of resistance corresponding the temperature identified in act (b), (d) determining a division ratio to be provided by a programmable voltage divider to force the resistance of the resistor to the value

calculated in act (c), and (e) configuring the programmable voltage divider to provide the division ratio determined in act (1).

Brief Description of the Drawings

5 Illustrative, non-limiting embodiments of the present invention are described by way of example with reference to the accompanying drawings, in which:

Fig. 1 is a constant current mass flow sensor according to the prior art;

Fig. 2 is a constant temperature mass flow sensor according to the prior art;

10 Fig. 3 is a constant temperature mass flow sensor that is capable of responding to changes in an ambient temperature of a fluid according to the prior art;

Fig. 4 is another constant temperature mass flow sensor that is capable of responding to changes in an ambient temperature of a fluid according to the prior art;

Fig. 5 is a constant temperature mass flow sensor according to one embodiment of the present invention;

15 Fig. 6A is a constant temperature mass flow sensor according to another embodiment of the present invention;

Fig. 6B is a flowchart of a temperature setting routine that may be used with the constant temperature mass flow sensor of Fig. 6A;

20 Fig. 7 is a constant temperature mass flow sensor according to yet another embodiment of the present invention;

Fig. 8 is a constant temperature mass flow sensor according to yet another embodiment of the present invention; and

Fig. 9 is a constant temperature mass flow sensor according to yet another embodiment of the present invention.

Detailed Description

25 Embodiments of the present invention will be understood more completely through the following detailed description which should be read in conjunction with the attached drawings in which similar reference numbers indicate similar structures.

30 Figs. 5, 6A, and 7-9 illustrate a number of different mass flow sensors according to various embodiments of the present invention. In each of Figs. 5, 6A, and 7-9, the reference designator R_1 represents the upstream coil, and reference designator R_2 represents the downstream coil. As in the prior art, coils R_1 and R_2 are disposed at spaced apart positions about a sensor conduit (not shown) through which a fluid flows. As defined herein, the term

fluid includes any material or combination of materials in a solid, liquid, or gaseous state. Each of coils R_1 and R_2 has a large and substantially identical thermal coefficient of resistance, such that the resistance of each coil R_1 , R_2 varies with temperature.

In contrast to the constant temperature mass flow sensors of Figs. 2-4, mass flow
5 sensors according to embodiments of the present invention do not use separate upstream and downstream circuits to independently set the temperature of the upstream and downstream coils to an identical value. Rather, embodiments of the present invention use a common circuit to set one of the upstream and downstream coils to a predetermined temperature or to a predetermined temperature above ambient, and then supply an amount of current to the
10 other of the upstream and downstream coils to force the resistance, and thus, the temperature, of the upstream and downstream coils to be equal. As a result, embodiments of the present invention do not require the close matching of component values and characteristics that is required in the separate upstream and downstream circuits of Figs. 2-4.

Fig. 5 illustrates a simplified schematic diagram of a mass flow sensor according to
15 one embodiment of the present invention. In broad overview, the circuit of Fig. 5 performs two main functions: setting the temperature of the downstream coil R_2 to a predetermined temperature, or to a predetermined temperature above the ambient temperature of the fluid flowing into the sensor conduit, and forcing the resistance value (and thus the temperature) of the upstream coil R_1 to equal that of the downstream coil R_2 . In operation, the circuit of Fig.
20 5 makes the resistance of the upstream coil R_1 equal to the resistance of the downstream coil R_2 , independently of the actual numeric value of resistance to which the downstream coil R_2 is set. It should be appreciated that the operation of the circuit of Fig. 5 may be reversed, such that the temperature of upstream coil R_1 is set to a predetermined temperature, or to a predetermined temperature above the ambient temperature of the fluid flowing into the sensor
25 conduit, and the resistance value (and thus, the temperature) of the downstream coil R_2 is forced to equal that of the upstream coil R_1 . As with the mass flow sensors of Figs 2-4, the difference in the amount of energy supplied to the upstream and downstream coils is proportional to the mass flow rate of the fluid flowing through the sensor conduit.

Referring to Fig. 5, current generated by a high gain operational amplifier 51 is
30 provided to two different resistive branches of the circuit; a first resistive branch being formed by the series connection of R' and R'' , and a second resistive branch formed by the series connection of R''' and R_2 . In the embodiment shown in Fig. 5, the output of the operational amplifier 51 is buffered by a transistor T_5 that is configured as an emitter-

follower and connected to a supply voltage V_{cc} by a resistor R . The combination of transistor T_5 and resistor R operates as a buffer circuit 55. Other types of buffer circuits may also be used, as the present invention is not limited to any particular implementation of buffer circuit 55. Moreover, it should be appreciated that depending on the output capabilities of the operational amplifier 51, the use of a buffer circuit may be omitted. Accordingly, although a buffer circuit 55 is depicted in each of Figs. 5, 6A, and 7-9, the present invention is not so limited.

One of the inputs of the operational amplifier 51 is connected between the series connection of R' and R'' of the first resistive branch, and the other is connected between the series connection of R''' and R_2 of the second resistive branch. In the embodiment shown in Fig. 5, the non-inverting (+) input of operational amplifier 51 is connected to the midpoint of the first resistive branch, and the inverting (-) input of the operational amplifier 51 is connected to the midpoint of the second resistive branch. In an alternative embodiment (not shown), the non-inverting (+) input of operational amplifier 51 is connected to the midpoint of the second resistive branch, with the inverting (-) input of the operational amplifier 51 being connected to the midpoint of the first resistive branch.

Connected to coil R_2 are coil R_1 , an adjustable current source 52 that provides an adjustable current ΔI , and a high gain operational amplifier 53. The inverting (-) input of operational amplifier 53 is connected to coil R_2 , coil R_1 , and the adjustable current source 52. Because the non-inverting (+) input of operational amplifier 53 is coupled to ground, the connection point between coil R_2 , coil R_1 , and the adjustable current source 52 is also at ground potential (i.e., is a "virtual ground"). Although not illustrated in Fig. 5, a buffer circuit similar to buffer circuit 55 may be connected between the output of operational amplifier 53 and coil R_1 , or alternatively, the operational amplifier 53 may include a buffered output stage.

The connection of the respective inputs of the operational amplifier 51 to the midpoint of each resistive branch, and the coupling of coil R_2 to a virtual ground forces the voltage at the midpoint of each resistive branch to be equal, with the result that $R'/R'' = R'''/R_2$. Thus, the first resistive branch of R' and R'' acts as a voltage divider that sets the ratio of R'''/R_2 .

By adjusting the value of the ratio R''/R' , the resistance, and thus, the temperature of coil R_2 may be set to any desired value. In one embodiment, resistor R'' includes a programmable resistor having a resistance value that is calculated to set the resistance, and thus, the temperature of coil R_2 to a predetermined value above the ambient temperature of the fluid flowing into the sensor conduit. Preferably, the temperature of coil R_2 is set

approximately 30° to 100° C above the ambient temperature of the fluid flowing into the sensor conduit, although the present invention is not limited to a particular value. In another embodiment, resistor R'' includes a resistor having a high thermal coefficient of resistance, such that when the ambient temperature of the fluid flowing into the sensor conduit changes, the resistance, and thus the temperature, of coil R₂ changes in a proportional manner. Of course it should be appreciated that because $R_2 = (R'' R''')/R'$, one or more of resistors R', R'', and R''' could alternatively include a variable or temperature dependent resistor. As described in detail further below, in a further embodiment of the present invention, the series combination of R' and R'' may be replaced by a programmable voltage divider that includes a digital to analog converter to set the resistance of coil R₂ to the desired value.

In operation, the circuit of Fig. 5 injects an amount of current ΔI to maintain the resistance, and thus, the temperature of coil R₁ equal to that of coil R₂. As a result, the following equations hold:

$$R_1 = V_1/I_1 \quad (1)$$

$$R_2 = V_2/I_2 \quad (2)$$

$$I_1 = \Delta I + I_2 \quad (3).$$

Accordingly,

$$\Delta I/I_2 = (V_1 - V_2)/V_2 \quad (4).$$

Thus, when the resistance (and thus, the temperature) of coil R₁ is equal to the resistance (and thus, the temperature) of coil R₂, the ratio of $\Delta I/I_2$ is equal to the difference between V₁ and V₂, divided by V₂, which is proportional to the mass flow rate of the fluid flowing through the sensor conduit.

As in the circuit of Figs. 2-4, the output voltages V₁ and V₂ may be provided to other processing circuits (not shown) that calculate, monitor, display, or regulate the mass flow rate of the fluid, based upon the values of output voltages V₁ and V₂. For example, output voltages V₁ and V₂ may be provided to the inputs of an amplifier, with the output of the amplifier and the output voltage V₂ being provided to a division circuit that forms the ratio $(V_1 - V_2)/V_2$. As these other processing circuits are well known and understood by those skilled in the art, the details of such processing circuits are omitted herein.

Advantageously, the circuit of Fig. 5 dispenses with the need for the close matching of corresponding components in separate upstream and downstream circuits that is required by the constant temperature and the constant temperature rise (above ambient) mass flow sensors of the prior art. For example, in each of the temperature sensors of Figs. 2-4, because

the resistance (and temperature) of the upstream and downstream coils are set to a particular numeric value by separate and independent upstream and downstream circuits, corresponding components in the upstream and downstream circuits must match and must vary in the same manner with respect to changes in the ambient temperature of the fluid. Any mismatch in component values and characteristics will be interpreted as a change in the rate of fluid flow. Thus, in the sensor of Fig. 4, R_1 must equal R_2 , R_3 must equal R_4 , R_5 must equal R_6 , R_7 must equal R_8 , the electrical characteristics of transistor 112 and differential amplifier 114 must match those of transistor 113 and differential amplifier 115, and the thermal characteristics of all components in the upstream circuit must match their corresponding components in the downstream circuit. In practice, such close matching of component values and characteristics is difficult to obtain, even with the use of precise (and expensive) components.

In contrast to the constant temperature mass flow sensors of the prior art, the mass flow sensor of Fig. 5 does not require a close matching of circuit components. In particular, as long as resistor R''' is stable over temperature, and as long as the ratio of R' to R'' is also stable over temperature (e.g., as long as the ratio $R'/R'' = K$, where K is a constant), the actual resistance values of resistors R' , R'' , and R''' are not critical. Furthermore, the circuit of Fig. 5, does not require that the downstream and upstream coils R_1 , R_2 be identical, as such identity is difficult to obtain in practice, and the actual temperature of coils R_1 and R_2 need not be identical at the same resistance value, as long as the difference in temperature between the two coils at the same resistance value is relatively constant for different values of resistance.

Fig. 6A illustrates a schematic diagram of a mass flow sensor according to another embodiment of the present invention. In Fig. 6A, that portion of the circuit designated by reference numeral 62 corresponds to one exemplary implementation of adjustable current source 52 in Fig. 5. The remaining portion of the circuit bearing reference numeral 61 corresponds to the remainder of the circuit in Fig. 5.

In a manner similar to that described with respect to Fig. 5, buffer 55 (which may include the emitter-follower circuit shown in Fig. 5) provides current generated by operational amplifier 51 to two resistive branches of the circuit; the first resistive branch including resistors R' and R'' , and the second resistive branch including resistor R''' and coil R_2 . As in the circuit of Fig. 5, one of the inputs of high gain operational amplifier 51 is connected between the series connection of R' and R'' of the first resistive branch, with the other being connected between the series connection of R''' and R_2 of the second resistive

branch. Connected to coil R_2 are coil R_1 and the inverting (-) input of high gain operational amplifier 53, with the non-inverting (+) input of operational amplifier 53 being coupled to ground. As in the circuit of Fig. 5, the connection of the respective inputs of the operational amplifier 51 to the midpoint of each resistive branch, and the coupling of coil R_2 to a virtual ground forces the voltage at the midpoint of each resistive branch to be equal, with the result that $R'/R'' = R'''/R_2$. Once again, the series connection of R' and R'' acts as a voltage divider, and by adjusting the value of R'' , the resistance, and thus, the temperature of coil R_2 may be set to any desired value.

In the embodiment illustrated in Fig. 6A, adjustable current source 52 (Fig. 5) includes

a unity gain instrumentation amplifier 63, a Digital to Analog Converter (DAC) 64, a unity gain operational amplifier 66, an Analog to Digital Converter (A/D) 65, and a proportional/integral/ differential (PID) controller 69.

Inverting (-) input of instrumentation amplifier 63 is connected to the inverting (-) input of operational amplifier 51 and voltage V_2 , and the non-inverting (+) input of instrumentation amplifier 63 is connected to the output of buffer 55. As a result of these connections, the output (V_{Ref}) of instrumentation amplifier 63 that is provided as the reference voltage input to DAC 64 is given by the following equation:

$$V_{Ref} = [(V_2 + I_2 R''') - V_2] = I_2 R''' \quad (5).$$

As known to those skilled in the art, the output voltage (V_{DAC}) of a digital to analog convertor is governed by the following relationship:

$$V_{DAC} = [V_{Ref} * X]/2^n \quad (6),$$

where V_{Ref} is the voltage reference input provided to the DAC, X is a digital input word provided to the DAC, and 2^n is the maximum permitted value of the input word X .

Accordingly, in Fig. 6A the output voltage provided by DAC 64 is given by the following equation:

$$V_{DAC} = [I_2 R''' * X]/2^n \quad (7).$$

Because the value of the current ΔI that is supplied by the adjustable current source 62 is equal to V_{DAC}/R , the following equation holds true when $R''' = R$:

$$\Delta I/I_2 = X/2^n \quad (8).$$

Referring now to the lower portion of Fig. 6A, a circuit is provided for generating a binary word X , that when provided as an input to DAC 64, causes the output of DAC 64 to provide an appropriate amount of current (ΔI) to coil R_1 so that the resistance of coil R_1

equals that of coil R_2 . As shown in Fig. 6A, the non-inverting (+) input of operational amplifier 66 receives voltage V_1 and the inverting (-) input of operational amplifier 66 receives voltage V_2 . The voltage V_2 is also provided as a reference voltage to the reference voltage input of A/D 65. Operational amplifier 66 therefore provides an output that is equal to the difference of V_1 and V_2 to the input of the A/D 65. A more detailed implementation of a circuit for providing the difference between V_1 and V_2 (i.e., $V_1 - V_2$) is illustrated in Fig. 6A by reference designator 66'.

As known to those skilled in the art, the binary output word X of an analog to digital convertor (A/D) is governed by the following relationship:

$$X = Y2^n/V_{\text{Ref}} \quad (9)$$

where V_{Ref} is the voltage reference input provided to the A/D, Y is the analog input voltage provided to the A/D, and 2^n is the maximum permitted binary value of the output word X . Accordingly, in Fig. 6A, the binary output word generated by the A/D 65 is given by the following equation:

$$X = (V_1 - V_2)2^n/V_2 \quad (10).$$

Substituting equation (10) into equation (8) yields the following:

$$\Delta I/I_2 = [(V_1 - V_2)2^n/V_2]/2^n = (V_1 - V_2)/V_2 \quad (11)$$

which is the same as equation 4. Thus, the A/D 65 generates a binary number X representing the ratio of $V_1 - V_2$ to V_2 , which, when provided to the input of DAC 64 after some additional processing, generates an appropriate amount of current ΔI to coil R_1 so that the resistance of coil R_1 equals that of coil R_2 .

As will be appreciated by those skilled in the art, when the number X is directly supplied as an input to DAC 64, the circuit of Fig. 6A will tend to be unstable. In particular, when going from a zero fluid flow state to a non-zero fluid flow state, and vice versa, the output X provided by the A/D 65 will cause the resistance of coil R_1 to diverge from that of R_2 . To correct this problem, the output (shown as X' in Fig. 6A) from A/D 65 may be input to a proportional/ integral/differential (PID) controller 69, with the output of the PID controller 69 being provided to the input X of DAC 64. In the circuit of Fig. 6A, the output X' of A/D 65 is provided to the feedback input of PID controller 69, with the output of the PID controller 69 being connected to the setpoint input of the PID controller 69. As the use and construction of a PID controller and similar types of control circuits are well known to those skilled in the art, further discussion of the PID controller 69 is omitted herein.

It should be appreciated that because the circuit of Fig. 6A forces the ratio of $\Delta I/I_2$ to be equal to the difference of V_1 and V_2 divided by V_2 , the circuit of Fig. 6A allows one to detect drift in the mass flow sensor. In particular, for a given change in ΔI , the quantity $(V_1 - V_2)/V_2$ changes proportionally, irrespective of the flow rate and ambient temperature of the fluid flowing into the sensor conduit. If at a time T_1 , a change in ΔI results in a particular value of change in the quantity $(V_1 - V_2)/V_2$, and at a later time T_2 , that same change in ΔI results in a different value of change in the quantity $(V_1 - V_2)/V_2$, it may be determined that the mass flow sensor has drifted. This is significant because in a typical mass flow sensor, it is nearly impossible to determine the difference between drift in the sensor and a change in the detected amount of flow. It should be appreciated that because it is possible to detect drift in the mass flow sensor circuit of Fig. 6A, a number of corrective actions may be taken. For example, upon the detection of drift in the sensor, an alert condition may be set to notify personnel that the sensor has drifted. The sensor may then be returned to the manufacturer for re-calibration. Alternatively, upon the detection of drift in the sensor, a correction factor may be supplied to compensate for the drift.

A flowchart of an exemplary temperature setting routine that may be used with the constant temperature mass flow sensor of Fig. 6A is now described with respect to Fig. 6B. As known to those skilled in the art, mass flow sensors frequently form but a portion of a mass flow controller. Other portions of the mass flow controller typically include one or more valves, a main flow path, and a processor (e.g., a CPU) that monitors and regulates the valves to control the amount of fluid flowing through the main flow path, according to the mass flow rate determined by the mass flow sensor.

According to one embodiment of the present invention, a temperature setting routine is provided that may be implemented in software that executes on a processor of a mass flow controller to set the value of resistance of one of the upstream R_1 and downstream R_2 coils of the sensor. After setting one of the upstream R_1 and downstream R_2 coils of the sensor to a particular value, the resistance balancing sensor circuits described with respect to Figs. 5 and 6A may be used to equalize the resistance of the other one of the upstream R_1 and downstream R_2 coils of the sensor. By then detecting the difference in the amount of energy supplied to each of the upstream R_1 and downstream R_2 coils when their resistance is equal, the mass flow rate of the fluid flowing in the conduit of the sensor, and thus, the mass flow rate of the fluid flowing in the main flow path may be determined. It should be appreciated that the temperature setting routine described below need not be implemented in software, but

may alternatively be implemented by a dedicated state machine or other control logic.

Moreover, it should also be appreciated that the temperature setting routine of Fig. 6B may be modified to set the temperature of one of the upstream R_1 and downstream R_2 coils to a predetermined temperature, rather than to a predetermined temperature above the ambient temperature of the fluid entering the sensor conduit.

At step 601 the temperature setting routine measures the ambient temperature of the fluid entering into the sensor conduit. This step may be performed, for example, by monitoring a thermometer (not shown) that is in thermal contact with the fluid entering into the sensor conduit, by monitoring a thermometer that is in thermal contact with the main fluid path, etc. After measuring the ambient temperature of the fluid entering into the sensor conduit, the routine proceeds to step 611, wherein the routine determines a temperature to which one of the upstream R_1 or downstream R_2 coils is set. For example, in the embodiment of Fig. 6A, where the downstream coil R_2 is set to a predetermined temperature based upon the value of $R_2 = (R'' R''')/R'$, and the amount of current ΔI is adjusted to set the resistance of the upstream coil R_1 equal to that of the downstream coil R_2 , the temperature to which the downstream coil R_2 is set may be based upon the following relationship:

$$T = T_{\text{Ambient}} + T_{\text{Rise}}, \quad (12),$$

where T_{Ambient} is the ambient temperature measured in step 601, and T_{Rise} is a fixed value, such as 30° to 100°C. In general the value of T_{Rise} should be at least several tens of degrees higher than the ambient temperature of the fluid entering into the sensor conduit, but not so high that it would create a problem with highly reactive fluids.

After determining the temperature to which the downstream coil R_2 is set in step 611, the routine proceeds to step 621. At step 621, the routine determines the appropriate value of resistance to which the downstream coil R_2 should be set based on the temperature of the coil (e.g., R_2) determined in step 611. As known to those skilled in the art, a second order approximation of the resistance of the coil is given by the following relationship:

$$R_{\text{coil}} = R_0(1 + \alpha T + \beta T^2) \quad (13),$$

where R_0 is the resistance of the coil (R_2) at 0°C, α and β are constants, and T is the desired temperature of the coil determined at step 611. After determining the coil resistance at step 621, the routine proceeds to step 631, wherein a division ratio that is to be set by the ratio of R''/R' is determined. As described above with respect to Fig. 6A, the division ratio may be set by adjusting the resistance of one or more variable resistors, by using a programmable voltage divider circuit that includes a Digital to Analog Converter (DAC), or in other ways

known to those skilled in the art. For example, the series combination of R' and R'' may be replaced by a DAC (not shown) having a voltage reference input that receives the output of buffer circuit 55, an output that is coupled to the non-inverting (+) input of operational amplifier 51, and an input that receives an appropriately valued input word X to provide the desired division ratio.

After determining the division ratio that is needed to set the resistance value of coil R_2 to the determined value, the routine proceeds to step 641, wherein the value of the ratio R''/R' determined at step 631 is set, and the routine terminates.

Fig. 7 illustrates a mass flow sensor according to another embodiment of the present invention. In contrast to the mass flow sensor of Fig. 6A, the mass flow sensor of Fig. 7 does not use a computational circuit to set the amount of current ΔI that is provided by the adjustable current source (e.g., adjustable current source 62 in Fig. 6A). Instead, the circuit of Fig. 7 balances currents in various resistive branches of the circuit to maintain the upstream coil R_1 and the downstream coil R_2 at the same resistance value.

In a manner similar to that described with respect to Figs. 5 and 6A, current from operational amplifier 51 is again provided to two resistive branches of the circuit via buffer 55; the first resistive branch including resistors R' and R'' , and the second resistive branch including resistor R''' and coil R_2 . As in the circuits of Figs. 5 and 6, one of the inputs of high gain operational amplifier 51 is connected between the series connection of R' and R'' of the first resistive branch, with the other being connected between the series connection of R''' and R_2 of the second resistive branch. Connected to coil R_2 are coil R_1 and the inverting (-) input of high gain operational amplifier 53, with the non-inverting (+) input of operational amplifier 53 being coupled to ground. As in the circuit of Figs. 5 and 6, the connection of the respective inputs of the operational amplifier 51 to the midpoint of each resistive branch, and the coupling of coil R_2 to a virtual ground forces the voltage at the midpoint of the first resistive branch to be equal to the voltage at the midpoint of the second resistive branch, with the result that $R'/R'' = R'''/R_2$. Once again, the series connection of R' and R'' acts as a voltage divider, and by adjusting the value of R'' , the resistance, and thus, the temperature of coil R_2 may be set to any desired value.

In contrast to the circuit of Fig. 6A, the circuit of Fig. 7 includes a large gain operational amplifier 71 having a non-inverting (+) input that is connected to the inverting (-) input of operational amplifier 51, and an inverting (-) input that is fed back from the output of the operational amplifier 71. In operation, the operational amplifier 71 acts as a buffer to

mirror the voltage V_2 and provide this voltage to R_2' . Connected to the midpoint of a third resistive branch formed by R_2' and R_1' is a high gain operational amplifier 72. The inverting (-) input of operational amplifier 72 is connected to the midpoint of the third resistive branch, with the non-inverting (+) input of operational amplifier 72 being coupled to ground. The output of operational amplifier 72 is fed back through R_1' and is also connected to coil R_1 . A fourth resistive branch is formed by the series connection of R_2 and R_1 . Operational amplifier 72 acts to force the voltage at the midpoint of the third resistive branch formed by R_2' and R_1' to be equal to that at the midpoint of the fourth resistive branch formed by R_2 and R_1 , with the result that the same proportional currents flow in R_2' and R_2 and in R_1' and R_1 . As a result, the ratio of $R_2'/R_1' = R_2/R_1$.

The remaining portion of the circuit of Fig. 7 designated by reference numeral 75 functions as an adjustable current source to provide an amount of current ΔI to the upstream coil R_1 so that the resistance of coil R_1 is equal to that of coil R_2 . As shown, resistor R_3 is connected between the inverting (-) input and the output of operational amplifier 53, resistor R_3' is connected between the output of operational amplifier 53 and the midpoint of the third resistive branch formed by R_2' and R_1' , and the non-inverting (+) input of operational amplifier 53 is coupled to ground.

The current at the midpoint of the fourth resistive branch formed by R_2 and R_1 is governed by the following relationship:

$$I_2 + \Delta I - I_1 = 0 \quad (14).$$

As $-V_o = \Delta I R_3$; $V_2 = I_2 R_2$; and $V_1 = I_1 R_1$; substituting these relationships into equation 14 yields the following relationship when $R_1 = R_2 = R$:

$$V_o = (V_2/R_2 - V_1/R_1) * R_3 = (V_2 - V_1) * R_3/R \quad (15); \text{ and}$$

$$\Delta I/I_2 = (V_2 - V_1)/V_2 \quad (16), \text{ which is the same}$$

relationship as that shown in equations 4 and 11.

As noted above, the circuit of Fig. 7 operates to provide an amount of current ΔI to the upstream coil R_1 so that the resistance of upstream coil R_1 is equal to that of the downstream coil R_2 . It should be appreciated that as the output V_o of operational amplifier 53 changes, the circuit of Fig. 7 remains in balance as long as the ratio of $R_1/R_1' = R_2/R_2' = R_3/R_3' = K$, where K is a constant. Thus, in contrast to the constant temperature mass flow sensors of the prior art, the circuit of Fig. 7 does not require the close matching of component values, as long as their ratios are equal and stable over temperature.

It should be appreciated that the circuit of Fig. 7 may be modified in a number of ways, without departing from the basic operation of the circuit. For example, high gain operational amplifier 71 may be replaced by a unity gain buffer. Alternatively, high gain operational amplifier 71 could be eliminated and resistor R_2' connected directly to the inverting (-) input of operational amplifier 51, such that the ratio of R'/R'' is equal to R''' divided by the parallel combination of R_2 and R_2' . Moreover, in Fig. 7, as well as in Figs. 5 and 6A, those connections that are shown as being coupled directly to ground may alternatively be coupled to ground through one or more resistors. It should also be appreciated that, as operational amplifiers 72 and 53 function to maintain the midpoints of the third and fourth resistive branches at a particular level, other circuit topologies may be used to achieve a similar result. For example, instead of the non-inverting (+) input of operational amplifier 72 being coupled to ground, this input may instead be connected to the midpoint of the fourth resistive branch formed by coils R_2 and R_1 , or alternatively, the non-inverting (+) input of operational amplifier 53 may instead be connected to the midpoint of the third resistive branch formed by resistors R_2' and R_1' . Each of these alternative configurations force the midpoints of the resistive branches to a known level that need not be at a ground potential. In addition, each of these alternative configurations help to reduce offset errors due to differences between operational amplifiers 53 and 72, although they may tend to make the circuit less stable.

The mass flow sensor of Fig. 7 is a constant temperature mass flow sensor, rather than a constant temperature rise (above ambient) sensor like that of Fig. 6A. As such, the circuit of Fig. 7 does not require any digital to analog converters or analog to digital converters. Of course it should be appreciated that the circuit of Fig. 7 may be modified to provide a constant temperature rise (above ambient) sensor, in a manner analogous to that of Fig. 6A. For example, digital to analog converters may be used to set the ratio of R''/R' and the ratio of R_3/R_3' to a desired value. Alternatively, one or more resistors (e.g., R'') having a high thermal coefficient of resistance may be used to automatically compensate for changes in the ambient temperature of the fluid flowing into the sensor conduit.

Fig. 8 illustrates a mass flow sensor according to another embodiment of the present invention. The mass flow sensor of Fig. 8 is similar in operation to the mass flow sensor previously described with respect to Fig. 7. However, large gain operational amplifier 71 has been replaced by a unity gain buffer 71' connected between the midpoint of the second resistive branch that includes R''' and R_2 , the inverting (-) input of operational amplifier 51,

and resistor R_2' . As a result, the inverting (-) input of operational amplifier 51 is connected directly to resistor R_2' , rather than being connected thereto via operational amplifier 71 as in Fig. 7. Unity gain buffer 71' mirrors voltage V_2 and provides this voltage to the third resistive branch formed by the series connection of R_2' and R_1' . As a result, the current through R_2' and R_2 and the current through R_1' and R_1 are equal with the result that the ratio of R_2'/R_1' is equal to R_2/R_1 .

In a manner similar to that of Fig. 7, the circuit of Fig. 8 operates to provide an amount of current ΔI to the upstream coil R_1 so that the resistance of coil R_1 is equal to that of coil R_2 . As the output V_o of operational amplifier 53 changes, the circuit of Fig. 8 also remains in balance as long as the ratio of $R_1/R_1' = R_2/R_2' = R_3/R_3'$. Thus, in contrast to the constant temperature mass flow sensors of the prior art, a close matching of components is not required.

Like the circuit of Fig. 7, the circuit of Fig. 8 may be modified in a number of ways, without departing from the basic operation of the circuit. Thus, for example, the non-inverting (+) input of operational amplifier 72 may be connected to the midpoint of the fourth resistive branch formed by coils R_2 and R_1 , rather than being coupled to ground, or alternatively, the non-inverting (+) input of operational amplifier 53 may be connected to the midpoint of the third resistive branch formed by resistors R_2' and R_1' , rather than being coupled to ground. Alternatively still, the circuit of Fig. 8 may be modified to provide a constant temperature rise (over ambient) mass flow sensor, rather than a constant temperature mass flow sensor. For example, the series combination of resistors R' and R'' may be replaced with a digital to analog converter having a reference voltage input that receives the output of operational amplifier 51, an output that is coupled to the non-inverting (+) input of operational amplifier 51, and an input that receives an appropriately valued input word to set the value of coil R_2 to the desired value. Similarly, another digital to analog converter may be used to adjust the ratio of R_3/R_3' to equal the value of R_2/R_2' (or alternatively, so that the ratio of $\Delta I/\Delta I'$ is equal to that of I_2/I_2'). This may be performed by adding a digital to analog converter between the output of operational amplifier 53 and resistor R_3 having a reference voltage input that receives the output of operational amplifier 53, an output that is coupled to resistor R_3 , and an input that receives an appropriately valued input word to set the value of coil R_3 to the desired value.

Fig. 9 illustrates a mass flow sensor according to another embodiment of the present invention. The mass flow sensor of Fig. 9 is similar in operation to the mass flow sensor

previously described with respect to Fig. 8. However, the configuration of operational amplifiers 53 and 72 in Fig. 9 is essentially the reverse of that in Fig. 8. In Fig. 9, the inverting (-) input of operational amplifier 72 is connected to the midpoint of the third resistive branch formed by R_2' and R_1' , with the non-inverting (-) input of operational amplifier 72 being coupled to ground. In contrast to the circuit of Fig. 8, however, the output of operational amplifier 72 is coupled through resistor R_3' to the midpoint of the fourth resistive branch formed by coil R_1 and coil R_2 , and is fed back to the inverting (-) input of operational amplifier 72 through resistor R_3 . The inverting (-) input of operational amplifier 53 is again connected to the midpoint of the fourth resistive branch formed by coil R_1 and coil R_2 , with the non-inverting (+) input of operational amplifier being coupled to ground. Thus, in Fig. 9, the portion of the circuit that provides the necessary amount of current ΔI to the upstream coil R_1 so that the resistance of coil R_1 is equal to that of coil R_2 includes operational amplifier 72 and resistors R_3 and R_3' . Advantageously, resistor R_3' may again be a variable resistor that can be set to a value that eliminates gain/temperature coefficients and provides a constant gain despite changes in the ambient temperature of the fluid flowing into the sensor conduit.

In a manner similar to that of Fig. 8, the circuit of Fig. 9 operates to provide an amount of current ΔI to the upstream coil R_1 so that the resistance of coil R_1 is equal to that of coil R_2 . Once again, as the output V_o of operational amplifier 53 changes, the circuit of Fig. 9 also remains in balance as long as the ratio of $R_1/R_1' = R_2/R_2' = R_3/R_3'$. Thus, in contrast to the constant temperature mass flow sensors of the prior art, a close matching of components is not required.

Like the circuit of Fig. 8, the circuit of Fig. 9 may also be modified in a number of ways, while preserving the basic operation of the circuit. Thus, for example, the non-inverting (+) input of operational amplifier 72 may be connected to the midpoint of the fourth resistive branch formed by coils R_2 and R_1 , rather than being coupled to ground, or alternatively, the non-inverting (+) input of operational amplifier 53 may be connected to the midpoint of the third resistive branch formed by resistors R_2' and R_1' , rather than being coupled to ground. Moreover, for certain applications, it may be preferable to reverse the connections of operational amplifier 72, so that the inverting (-) input of operational amplifier 72 is coupled to ground with the non-inverting (+) input being connected to the midpoint of the third resistive branch formed by resistors R_2' and R_1' . Like the circuits of Figs. 7 and 8,

the circuit of Fig. 9 may be modified to use digital to analog converters that can adjust and/or set the values of R_2 and R_3 to a desired value.

It should be appreciated that each of the mass flow sensors of Figs. 5, 6A, and 7-9 may benefit from the use of one or more stabilizing circuits that improve the transient
5 response of sensor without overshoot or ringing. As there are a wide variety of stabilizing circuits that are well known in the art and which may be used in conjunction with the mass flow sensors described with respect to Figs 5, 6A, and 7-9, a detailed description such circuits is omitted herein.

Although embodiments of the present invention have been described in terms of
10 setting a temperature and thus, the resistance, of the downstream coil to a predetermined value and then adjusting an amount of current provided to the upstream coil to equal the resistance and thus, the temperature of the downstream coil, it should be appreciated that the present invention is not so limited. In this regard, the positions of coils R_1 and R_2 in the
circuits of Figs. 5, 6A, and 7-9 may be reversed, such that these circuits set the temperature
15 (and thus, the resistance) of the upstream coil to a predetermined value and then adjust the amount of current provided to the downstream coil to equal the resistance, and thus the temperature, of the upstream coil.

Further, although embodiments of the present invention have been described with
respect to a mass flow sensor that is particularly well suited for semiconductor manufacturing
20 processes, it should be appreciated that embodiments of the present invention may be used in other applications and processes. For example, embodiments of the present invention may be used in automotive applications to measure the amount of a fluid such as gasoline, or diesel fuel, or air that is delivered to a combustion chamber. Moreover, embodiments of the present
invention are not limited to mass flow sensors, as the present invention may be used in other
25 sensor and detection circuits. For example, embodiments of the present invention may be readily adapted for use in a hot-wire anemometer or any other applications in which variations in the resistance of a leg of a resistive bridge circuit is indicative of a change in a property that varies with resistance.

Having described several embodiments of the invention in detail, various
30 modifications and improvements will readily occur to those skilled in the art. Such modifications and improvements are intended to be within the scope of the invention. Accordingly, the foregoing description is by way of example only, and is not intended as

limiting. The invention is limited only as defined by the following claims and the equivalents thereto.

CLAIMS

1. A sensor, comprising:
a first resistor and a second resistor each having a resistance that varies in response to a change in a physical property;
5 a first circuit, electrically coupled to the first resistor, that sets the resistance of the first resistor; and
a second circuit, electrically coupled to the second resistor, that adjusts the resistance of the second resistor to equal the resistance of the first resistor.

10 2. The sensor of claim 1, further comprising:
a processing circuit, coupled to the first and second circuits, that measures a difference in an amount of energy provided by the first and second circuits to the first and second resistors, respectively.

15 3. The sensor of claim 1, wherein the second circuit adjusts the resistance of the second resistor by changing the amount of current provided to the second resistor.

20 4. The sensor of claim 1, wherein the sensor is a mass flow sensor that measures a mass flow rate of a fluid that flows through a conduit about which the first and second resistors are disposed.

25 5. The sensor of claim 4, wherein a resistance value to which the first resistor is set corresponds to a temperature that is above an ambient temperature of the fluid entering the conduit.

6. The sensor of claim 4, wherein a resistance value to which the first resistor is set corresponds to a temperature that is approximately 30 to 100 degrees Celsius above an ambient temperature of the fluid entering the conduit.

30 7. The sensor of claim 1, wherein the resistance of the first and second resistors varies in response to a change in temperature.

8. The sensor of claim 1, wherein the first circuit includes a programmable voltage divider that sets the resistance of the first resistor.

9. The sensor of claim 1, wherein the first circuit includes a digital to analog converter that sets the resistance of the first resistor.

5

10. The sensor of claim 1, wherein the first circuit includes:
an amplifier having first and second inputs and an output;
a voltage reference, electrically coupled to the first input of the amplifier, that determines the resistance to which the first resistor is set; and
10 a third resistor, electrically coupled between the second input of the amplifier and the output of the amplifier;
wherein the first resistor is electrically coupled in series between the second and third resistors.

15 11. The sensor of claim 10, wherein the voltage reference includes a programmable voltage divider.

12. The sensor of claim 10, wherein the amplifier is a first amplifier, and wherein the second circuit includes:

20 a second amplifier having first and second inputs and an output, the first input of the second amplifier being electrically coupled to a reference potential terminal, the second input being electrically coupled to the first and second resistors, and the second resistor being electrically coupled between the second input of the second amplifier and the output of the second amplifier; and

25 a current source that is electrically coupled to the second input of the second amplifier and to the first and second resistors.

13. The sensor of claim 12, wherein the current source includes:

a digital to analog converter having an output; and

30 a fourth resistor that is electrically coupled between the output of the digital to analog converter and the second input of the second amplifier.

14. The sensor of claim 13, wherein the current source further includes:

an analog to digital converter having an input and output; and
a proportional/integral/differential controller having an input that is electrically coupled to the output of the analog to digital converter and having an output that is electrically coupled to the input of the digital to analog converter.

5

15. The sensor of claim 12, further comprising:

a buffer that electrically couples the first and third resistors to the second input of the first amplifier, and

a fourth resistor and a fifth resistor electrically coupled in series between the second input of the first amplifier and the output of the second amplifier.

10

16. The sensor of claim 15, wherein the reference potential terminal is a first reference potential terminal, and wherein the current source includes:

a third amplifier having first and second inputs and an output, the first input of the third amplifier being electrically coupled to a second reference potential terminal having a same reference potential as the first reference potential terminal;

15

a sixth resistor that is electrically coupled between the output of the third amplifier, the first and second resistors, and the second input of the second amplifier; and

a seventh resistor that is electrically coupled between the output of the third amplifier and the fourth and fifth resistors.

20

17. The sensor of claim 10, wherein the amplifier is a first amplifier and the second circuit includes:

a second amplifier having first and second inputs and an output, the first input of the second amplifier being electrically coupled to a reference potential terminal;

25

a fourth resistor and a fifth resistor that are electrically coupled in series between the second input of the first amplifier and the output of the second amplifier, the second input of the second amplifier being electrically coupled to the fourth and fifth resistors; and

a current source that is electrically coupled to the first and second resistors.

30

18. The sensor of claim 17, wherein the reference potential terminal is a first reference potential terminal, and wherein the current source includes:

a third amplifier having first and second inputs and an output, the first input of the third amplifier being electrically coupled to a second reference potential terminal having a same reference potential as the first reference potential terminal;

a sixth resistor that is electrically coupled between the output of the third amplifier and the second input of the third amplifier, the sixth resistor being electrically coupled to the first and second resistors; and

a seventh resistor that is electrically coupled between the output of the third amplifier and the second input of the second amplifier, the seventh resistor being electrically coupled to the fourth and fifth resistors.

19. A mass flow sensor comprising:

a first heat sensitive coil and a second heat sensitive coil disposed at spaced apart positions about a conduit through which a fluid flows, the first and second heat sensitive coils each having a resistance that varies with temperature;

a first circuit, electrically coupled to the first heat sensitive coil, that sets the resistance of the first heat sensitive coil to a value that corresponds to a predetermined temperature;

a second circuit, electrically coupled to the second heat sensitive coil, that adjusts an amount of current provided to the second heat sensitive coil so that the resistance of the second heat sensitive coil equals the resistance of the first heat sensitive coil; and

a processing circuit, coupled to the first and second circuits, that measures a difference in an amount of energy provided by the first and second circuits to the first and second heat sensitive coils, respectively.

20. The mass flow sensor of claim 19, wherein the value of resistance to which the first heat sensitive coil is set corresponds to a predetermined temperature that is above an ambient temperature of the fluid entering the conduit.

21. The mass flow sensor of claim 19, wherein the value of resistance to which the first heat sensitive coil is set corresponds to a predetermined temperature that is approximately 30 to 100 degrees Celsius above an ambient temperature of the fluid entering the conduit.

22. The mass flow sensor of claim 19, wherein the first circuit includes:

an amplifier having first and second inputs and an output;
a voltage reference, electrically coupled to the first input of the amplifier, that
determines the resistance to which the first heat sensitive coil is set; and
a first resistor, electrically coupled between the second input of the amplifier and the
5 output of the amplifier;
wherein the first heat sensitive coil is electrically coupled in series between the
second heat sensitive coil and first resistor.

23. The mass flow sensor of claim 22, wherein the amplifier is a first amplifier,
10 and wherein the second circuit includes:

a second amplifier having first and second inputs and an output, the first input of the
second amplifier being electrically coupled to a reference potential terminal, the second input
being electrically coupled to the first and second heat sensitive coils, and the second heat
sensitive coil being electrically coupled between the second input of the second amplifier and
15 the output of the second amplifier; and

a current source that is electrically coupled to the second input of the second amplifier
and to the first and second heat sensitive coils.

24. The mass flow sensor of claim 23, wherein the current source includes:
20 a digital to analog converter having an output; and
a second resistor that is electrically coupled between the output of the digital to analog
converter and the second input of the second amplifier.

25. The mass flow sensor of claim 24, wherein the current source further includes:
an analog to digital converter having an input and output; and
25 a proportional/integral/differential controller having an input that is electrically
coupled to the output of the analog to digital converter and having an output that is
electrically coupled to the input of the digital to analog converter.

26. The mass flow sensor of claim 25, wherein the mass flow sensor is included in
30 a mass flow controller.

27. The mass flow sensor of claim 23, further comprising:

a buffer that electrically couples the first heat sensitive coil and the first resistor to the second input of the first amplifier, and

a second resistor and a third resistor electrically coupled in series between the second input of the first amplifier and the output of the second amplifier.

5

28. The mass flow sensor of claim 27, wherein the reference potential terminal is a first reference potential terminal, and wherein the current source includes:

a third amplifier having first and second inputs and an output, the first input of the third amplifier being electrically coupled to a second reference potential terminal having a same reference potential as the first reference potential terminal;

10

a fourth resistor that is electrically coupled between the output of the third amplifier, the first and second heat sensitive coils, and the second input of the second amplifier; and

a fifth resistor that is electrically coupled between the output of the third amplifier and the second and third resistors.

15

29. The mass flow sensor of claim 28, wherein the mass flow sensor is included in a mass flow controller.

30. The mass flow sensor of claim 22, wherein the amplifier is a first amplifier and the second circuit includes:

20

a second amplifier having first and second inputs and an output, the first input of the second amplifier being electrically coupled to a reference potential terminal;

a second resistor and a third resistor that are electrically coupled in series between the second input of the first amplifier and the output of the second amplifier, the second input of the second amplifier being electrically coupled to the second and third resistors; and

25

a current source that is electrically coupled to the first and second heat sensitive coils.

31. The mass flow sensor of claim 30, wherein the reference potential terminal is a first reference potential terminal, and wherein the current source includes:

a third amplifier having first and second inputs and an output, the first input of the third amplifier being electrically coupled to a second reference potential terminal having a same reference potential as the first reference potential terminal;

30

a fourth resistor that is electrically coupled between the output of the third amplifier and the second input of the third amplifier, the fourth resistor being electrically coupled to the first and second heat sensitive coils; and

5 a fifth resistor that is electrically coupled between the output of the third amplifier and the second input of the second amplifier, the fifth resistor being electrically coupled to the second and third resistors.

32. The mass flow sensor of claim 31, wherein the mass flow sensor is included in a mass flow controller.

10 33. A method of balancing a resistance of a first resistor and a resistance of a second resistor, the resistance of the first and second resistors varying with temperature, the method comprising acts of:

- 15 (a) setting the resistance of the first resistor to a first value; and
(b) providing an amount of current to the second resistor so that the resistance of the second resistor matches the first value of the first resistor.

34. The method of claim 33, wherein act (a) includes acts of:
(c) determining a temperature to which the first resistor is to be set; and
20 (d) setting the resistance of the first resistor to a value of resistance that corresponds to the temperature determined in act (c).

35. The method of claim 34, wherein act (c) includes acts of:
(e) measuring an ambient temperature of a fluid flowing into a conduit about which
25 the first resistor and the second resistor are disposed; and
(f) incrementing the ambient temperature measured in act (e) by a predetermined amount.

36. The method of claim 35, wherein act (d) includes acts of:
30 (g) determining a division ratio to be provided by a programmable voltage divider to force the resistance of the first resistor to the first value; and
(h) configuring the programmable voltage divider to provide the determined division ratio.

37. A method of setting the resistance of a resistor, comprising acts of:

(a) measuring an ambient temperature of a fluid flowing into a conduit about which the resistor is disposed;

5 (b) incrementing the ambient temperature measured in act (a) by a predetermined amount to identify a temperature to which the resistor is to be set;

(c) calculating a value of resistance corresponding the temperature identified in act (b);

10 (d) determining a division ratio to be provided by a programmable voltage divider to force the resistance of the resistor to the value calculated in act (c); and

(e) configuring the programmable voltage divider to provide the division ratio determined in act (d).

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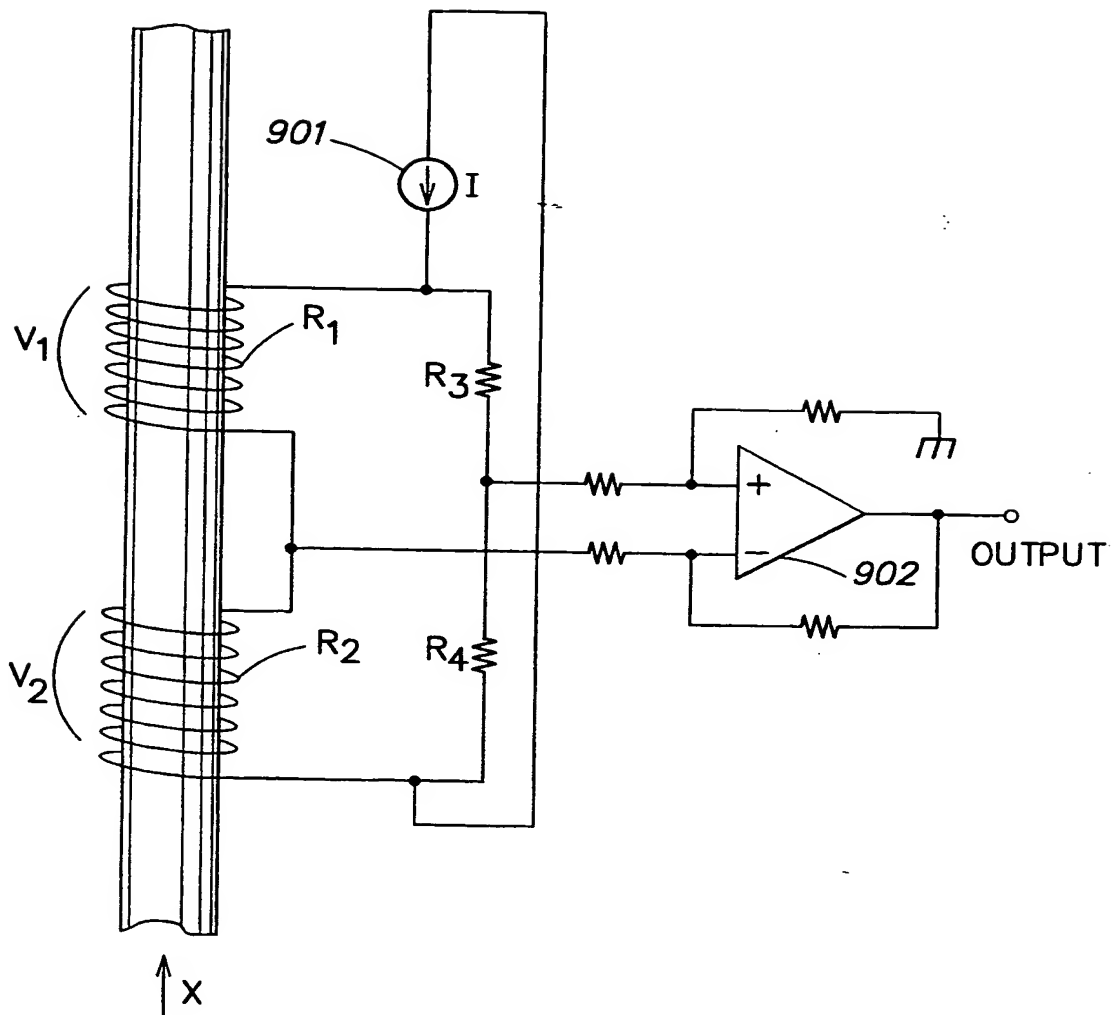
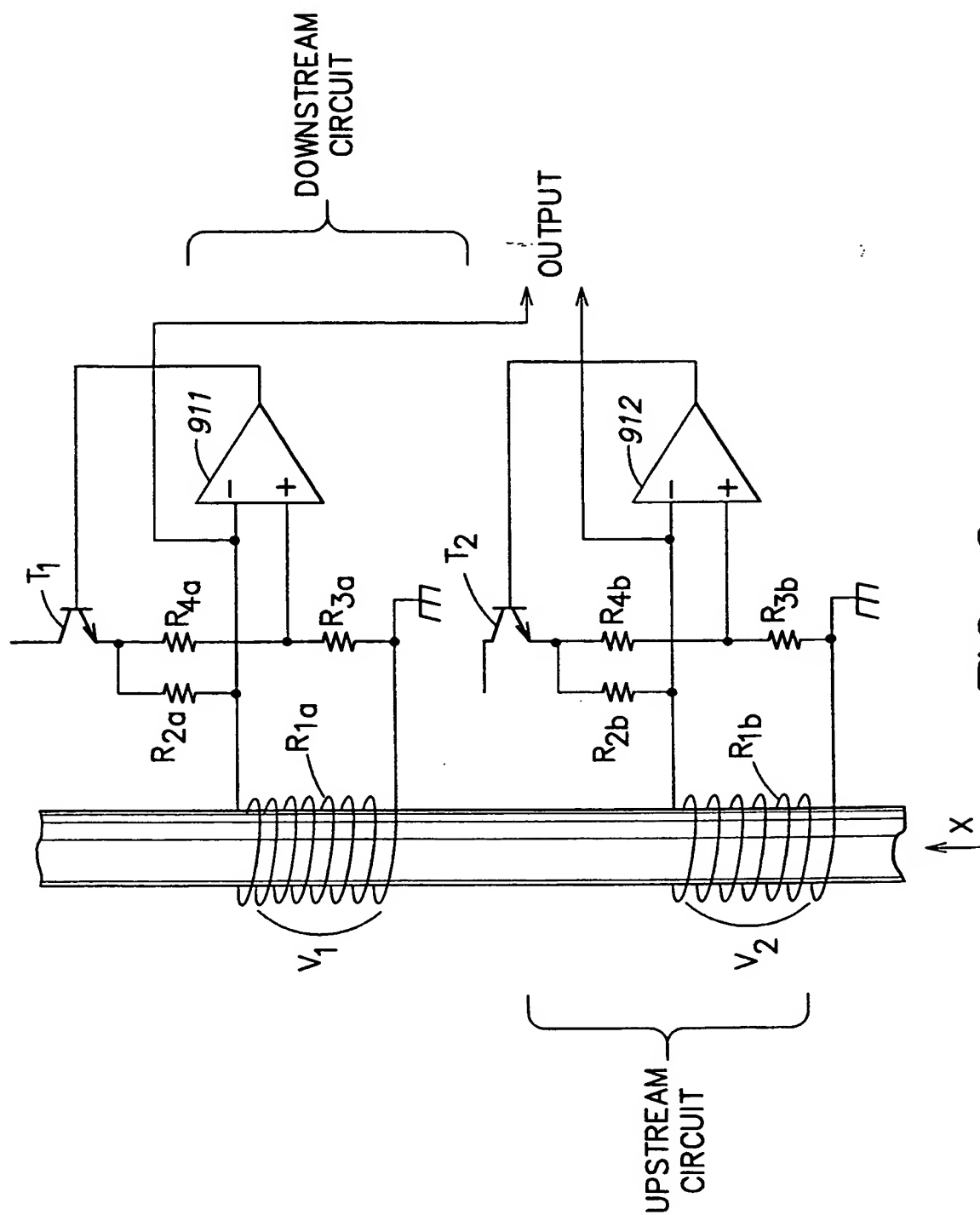


FIG. 1
(PRIOR ART)

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**FIG. 2**
(PRIOR ART)

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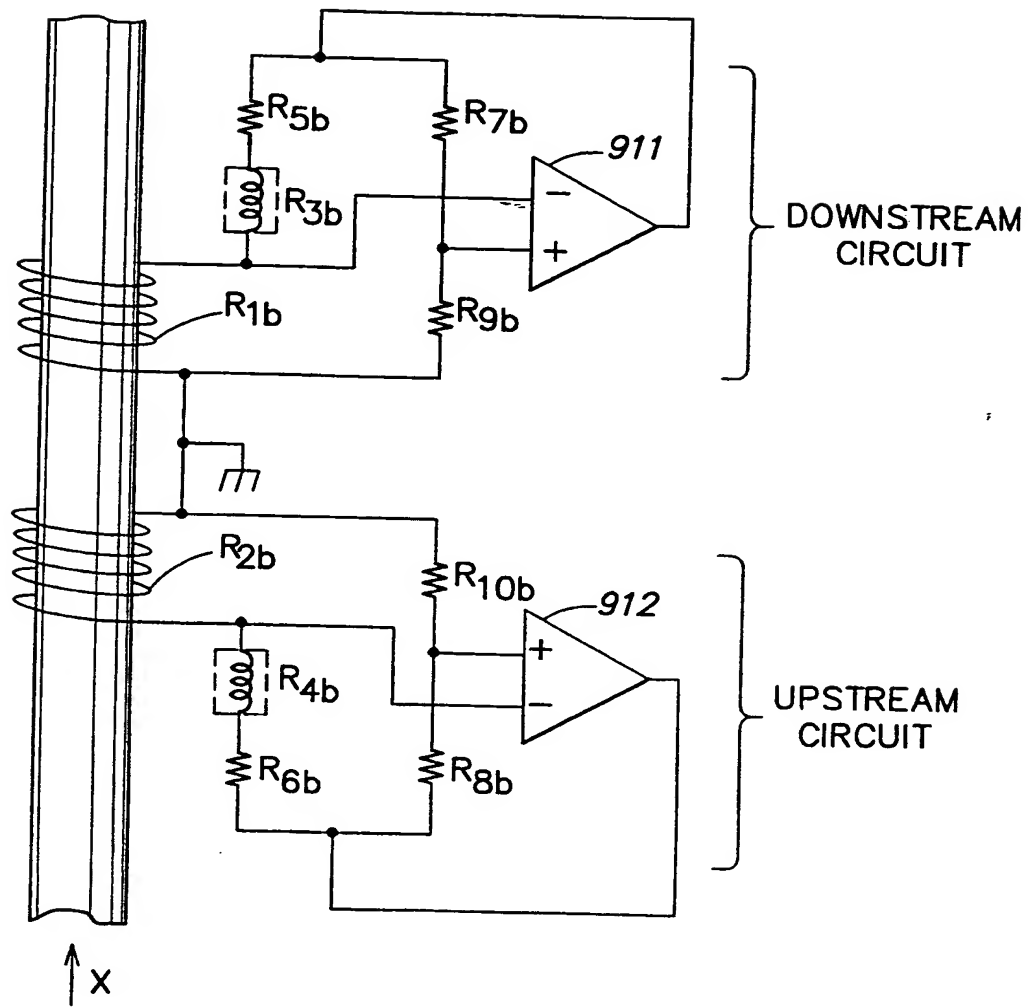


FIG. 3
(PRIOR ART)

SUBSTITUTE SHEET (RULE 26)

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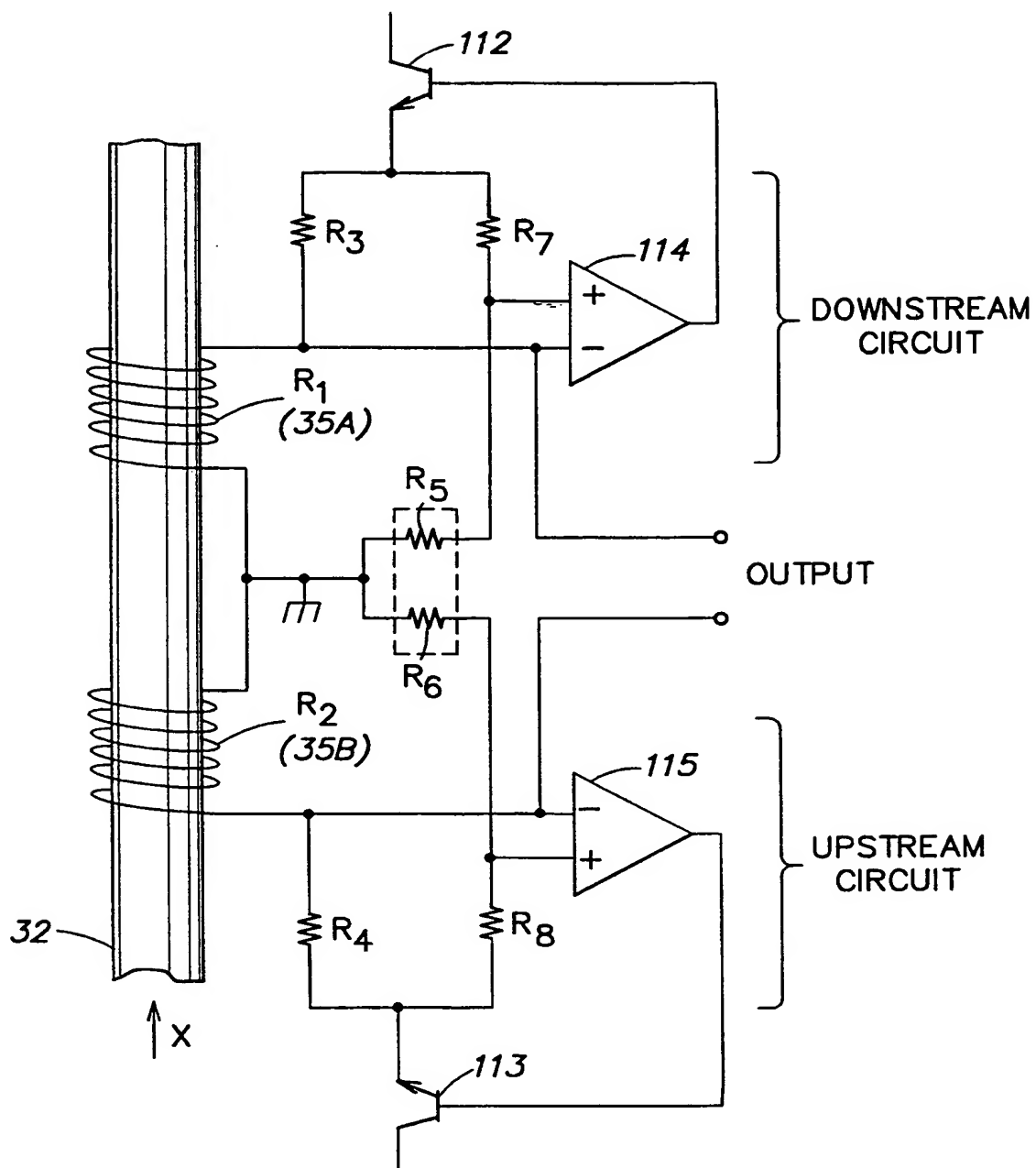


FIG. 4
(PRIOR ART)

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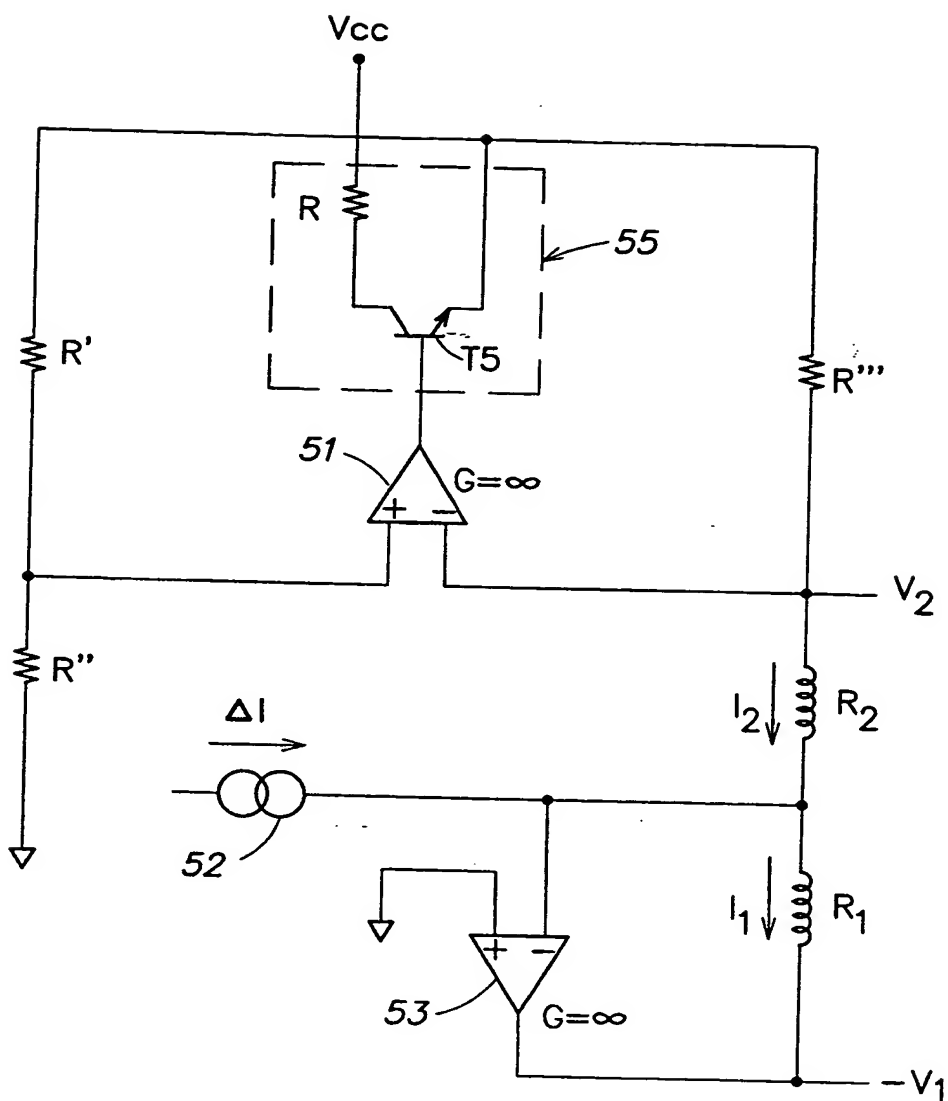


FIG. 5

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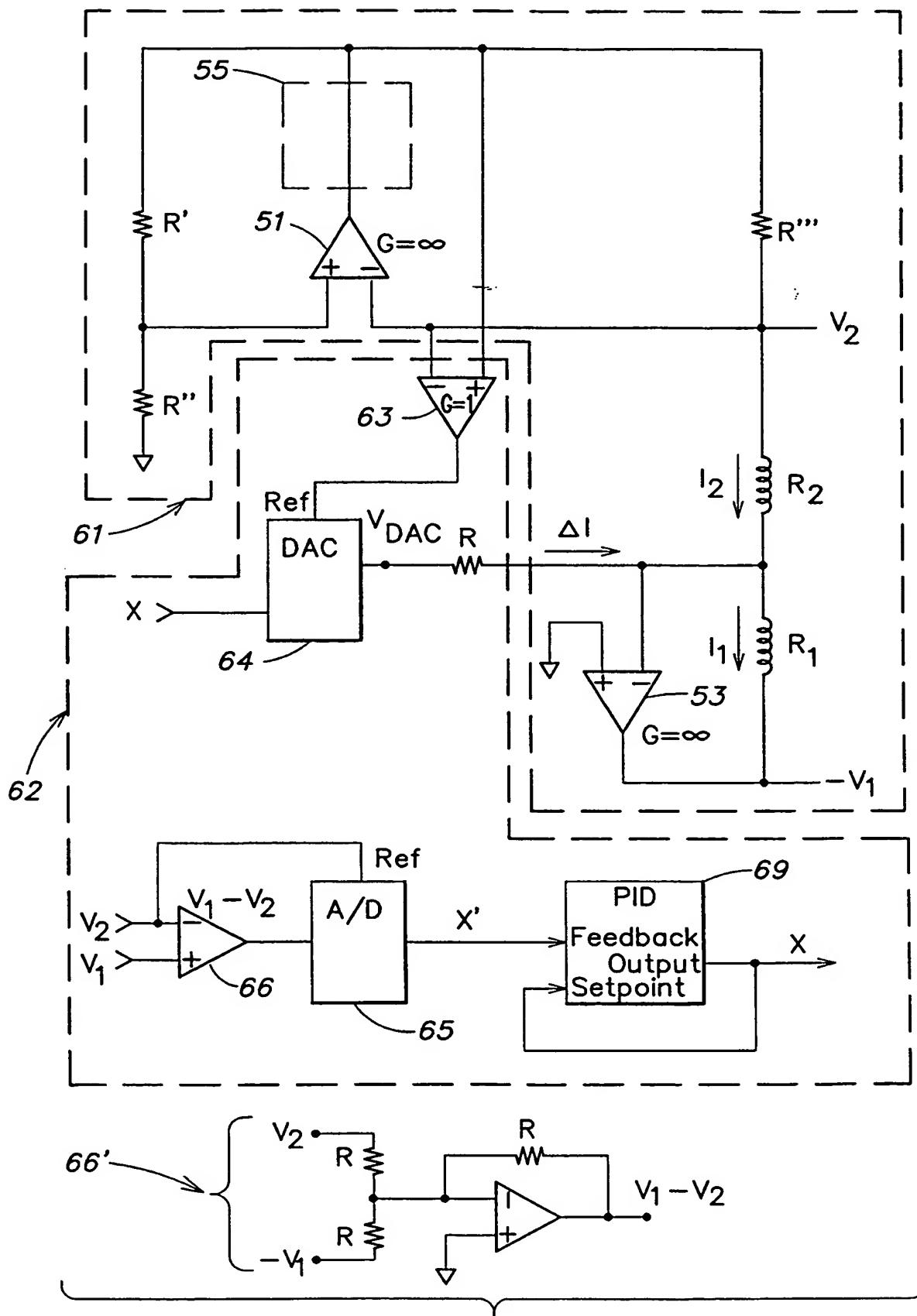
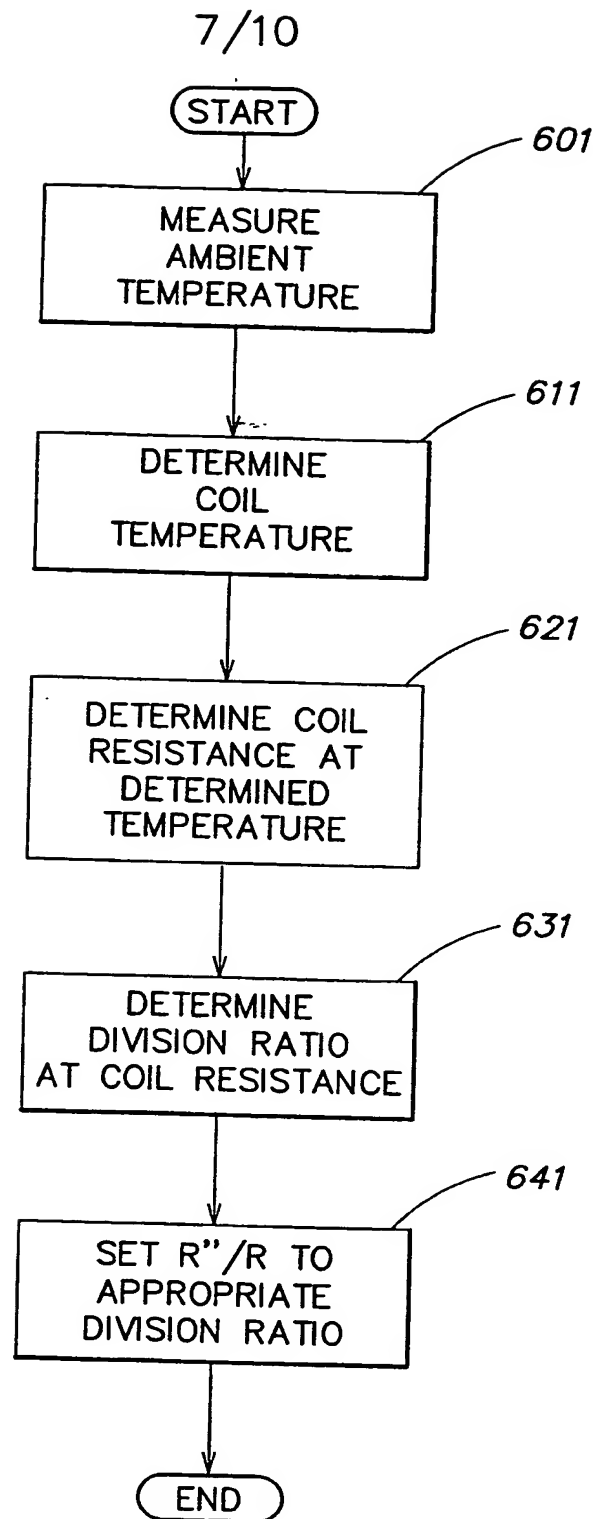


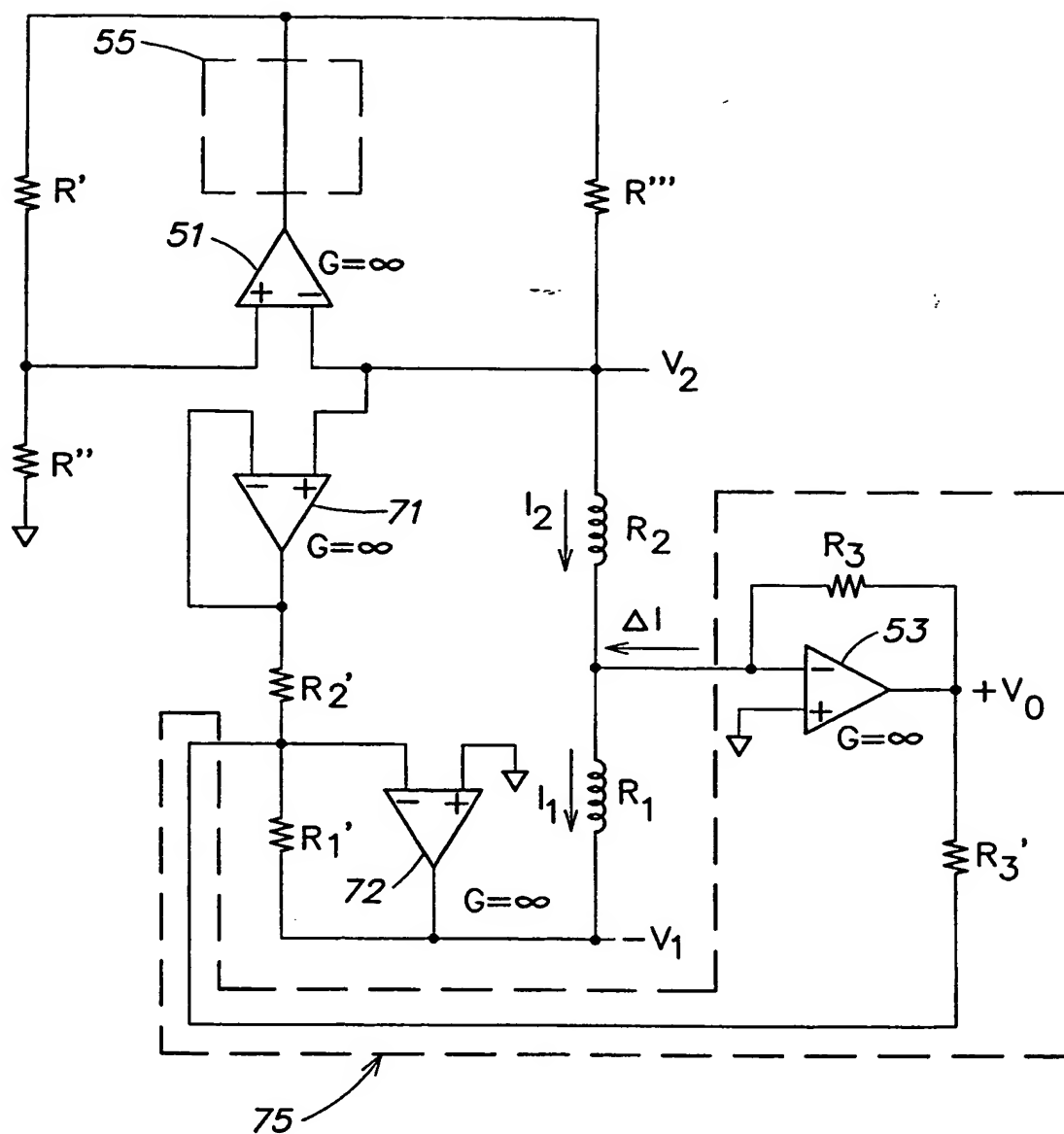
FIG. 6A

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**FIG. 6B**

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**FIG. 7**

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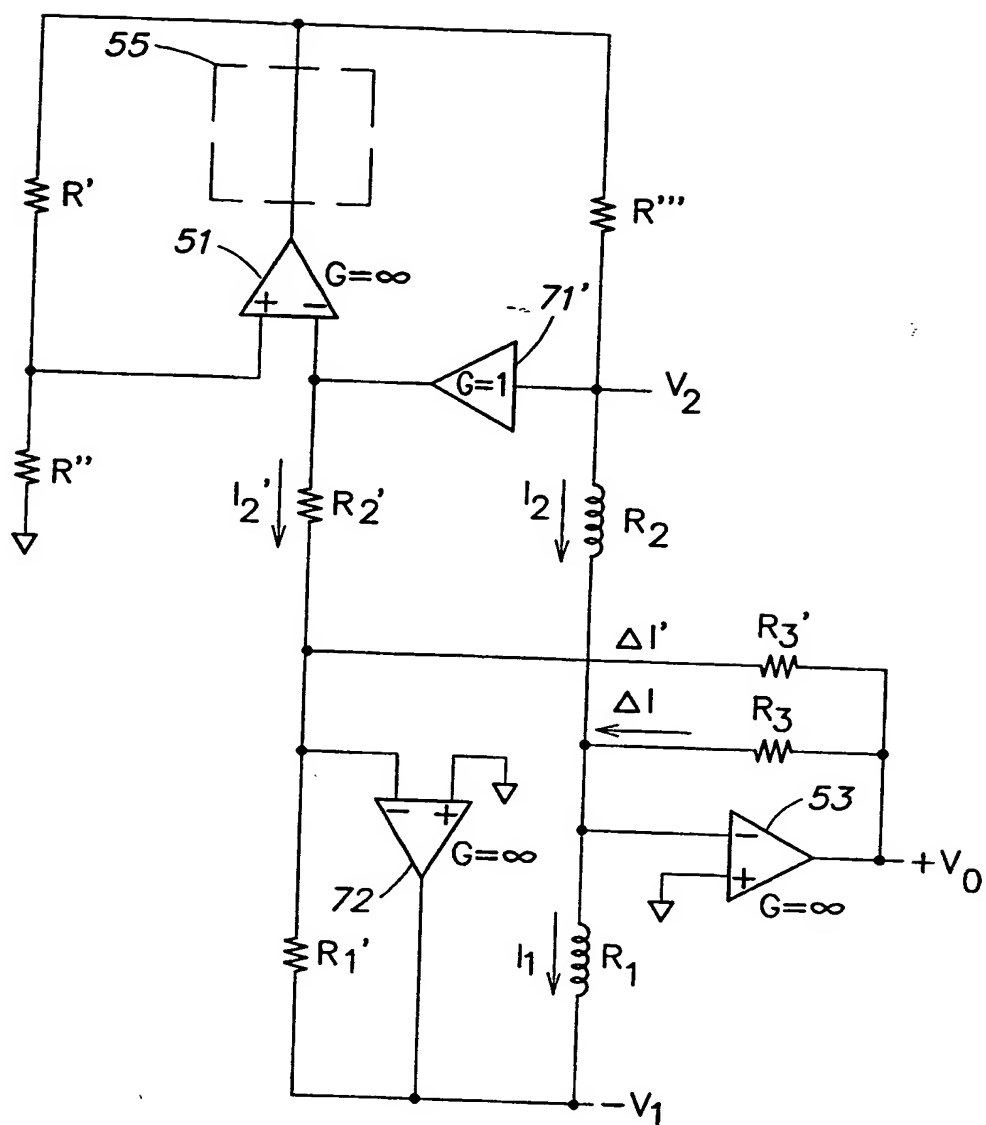
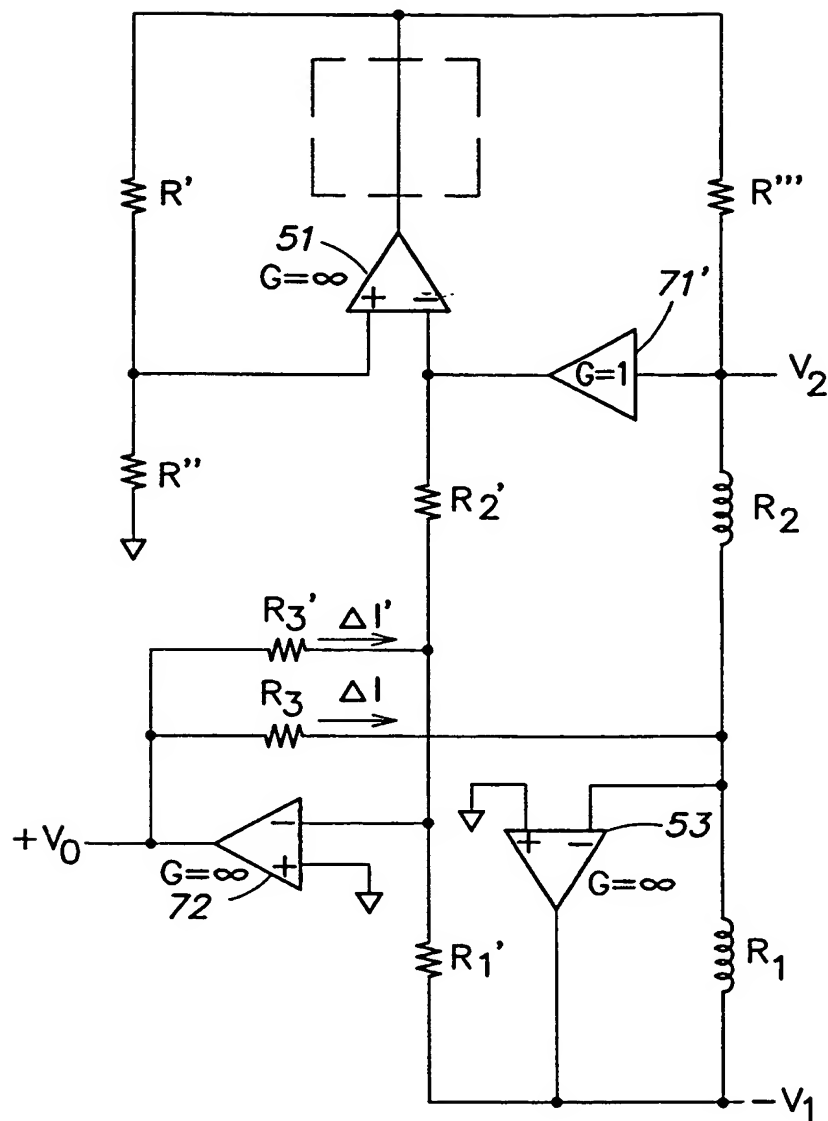


FIG. 8

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**FIG. 9**

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INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 01/04609

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 G01F1/684 G01F1/696 G01F1/698 G01F1/86

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G01F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, PAJ, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 843 881 A (HUBBARD ARTHUR C) 4 July 1989 (1989-07-04) abstract column 4, line 24 - line 46; figures 1,2	1,2,19, 20,33
A		37
A	US 5 410 912 A (SUZUKI ISAO) 2 May 1995 (1995-05-02) abstract; figure 9	1,19,33, 37

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

28 May 2001

Date of mailing of the international search report

05/06/2001

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Vorropoulos, G

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 01/04609

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
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US 5410912	A	02-05-1995	JP 4366725 A	18-12-1992
			JP 8016623 B	21-02-1996
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